

Optimal and Robust controller Synthesis

Using Energy Timed Automata with Uncertainty

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Presentation based on a paper accepted for publication at Formal Methods (FM'18)

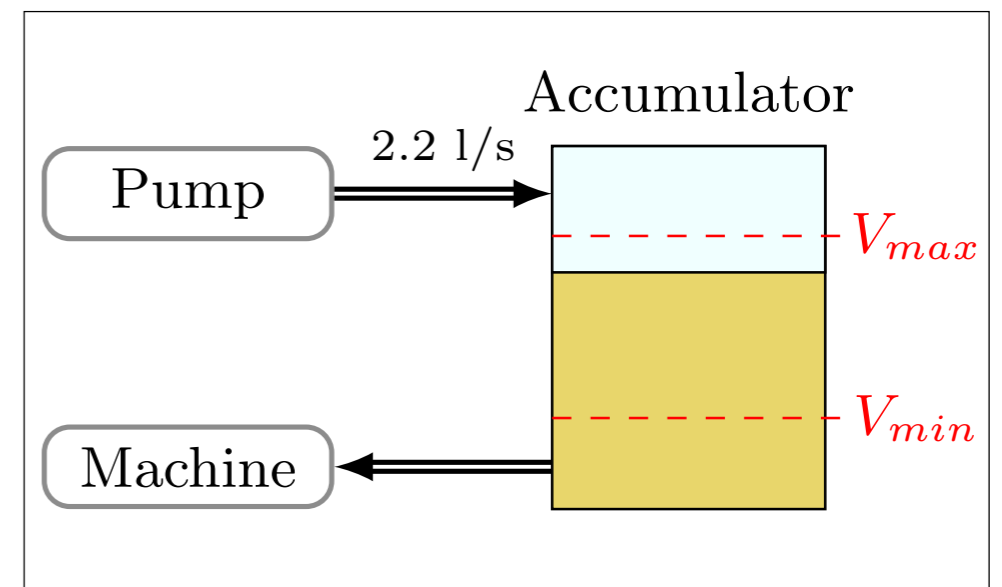
Work supported by ERC projects LASSO and EQualls



Industrial Example: the HYDAC system

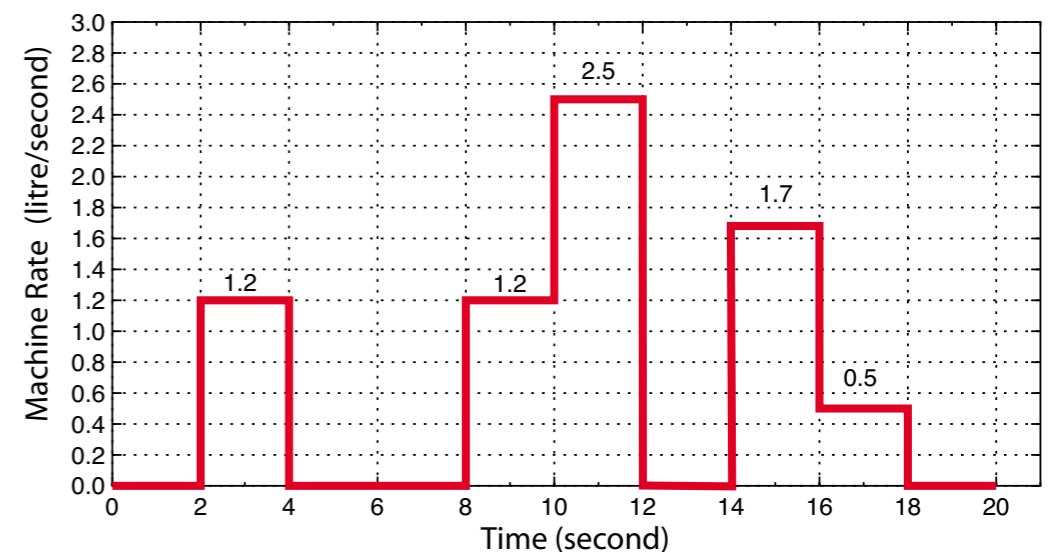
System components

- A **machine** that consumes oil according to a fixed cyclic pattern of 20 s
- Hydraulic **accumulator** containing oil and a fixed amount of gas that puts the oil under pressure
- **Controllable pump** (on/off) which pumps oil into the accumulator with rate 2.2 l/s



The control objective

- The level of oil shall be maintained within a **safe interval** $[V_{max}; V_{min}] = [4.9; 25.1]$ l
- The system shall **never stop**
- The controller shall **minimise the average level of oil** so that the oil pressure is kept as low as possible



Motivation

- Automatic synthesis of controllers for embedded systems is a difficult task
- They need to satisfy safety properties involving non-functional aspects such as time constraints and limited resources
- While ensuring optimality w.r.t. given performance objectives

Energy constraints

GOMSPACE



Our contribution

- Novel framework for **automatic synthesis of safe & optimal controllers** for **resource-aware** systems modelled as **energy timed automata**
- Controller synthesis are obtained by solving **time- and energy-constrained infinite run problems**
- We address an open problem from [Bouyer, Fahrenberg, Larsen, Markey, Srba — FORMATS'08]

Context

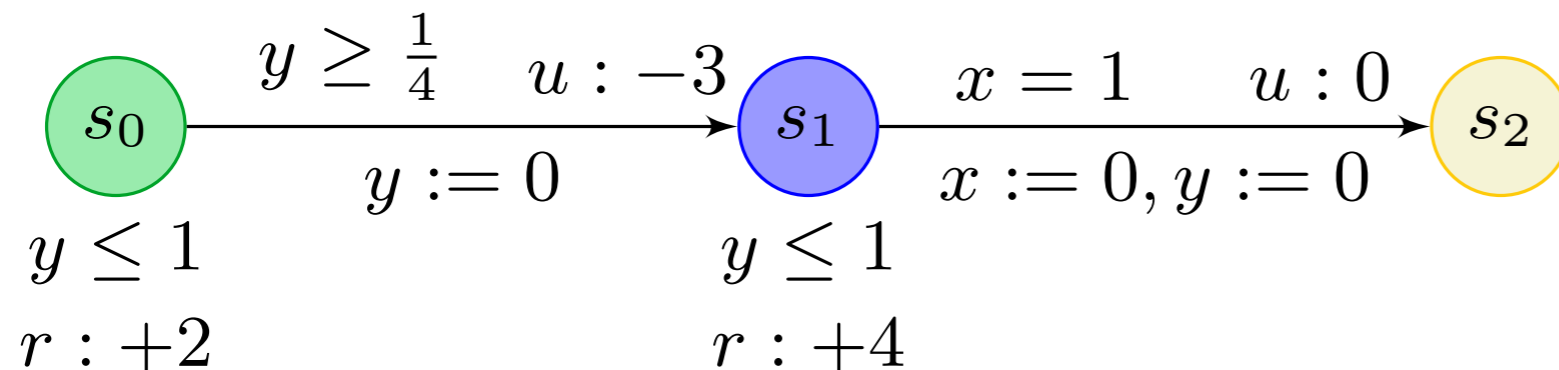
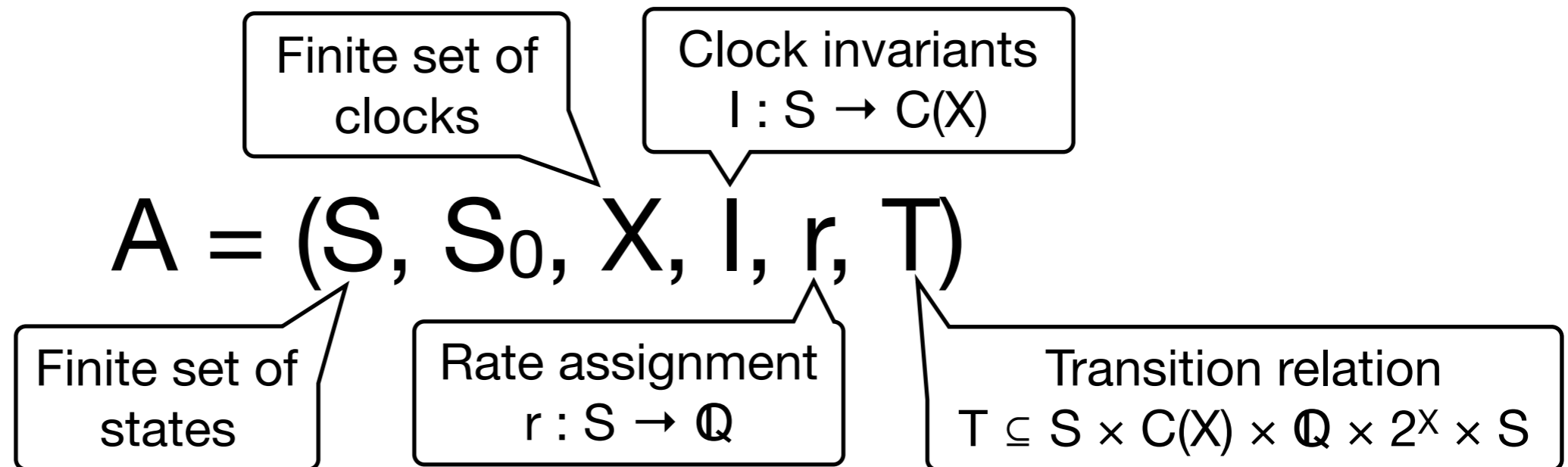
Untimed

	games	existential problem	universal problem
L	$\in UP \cap coUP$ P-h	$\in P$	$\in P$
L+W	$\in NP \cap coNP$ P-h	$\in P$	$\in P$
L+U	EXPTIME-c	$\in PSPACE$ NP-h	$\in P$

1 Clock

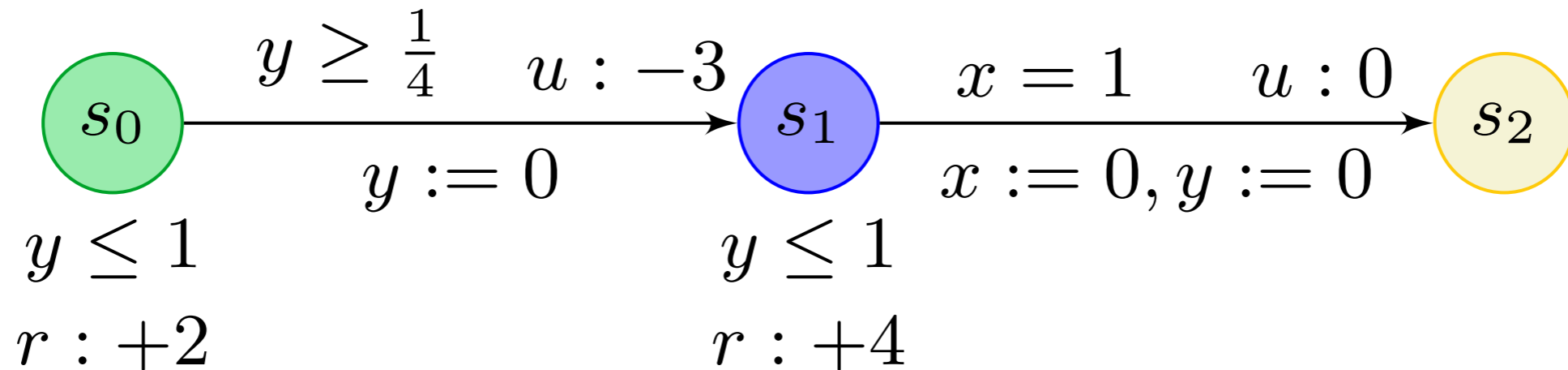
	games	existential problem	universal problem
L	?	$\in P$	$\in P$
L+W	?	$\in P$	$\in P$
L+U	undecidable	?	?

Energy Timed Automata

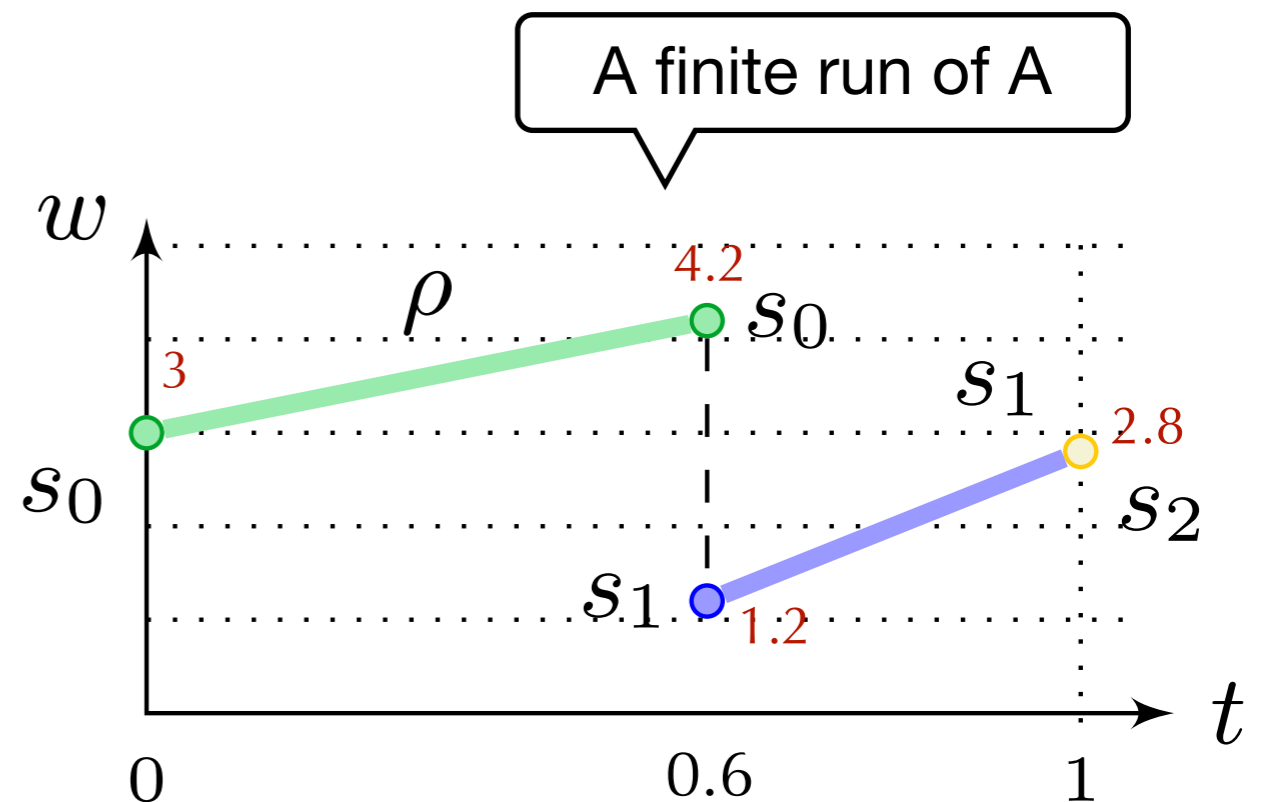


An ETA is an **Energy Timed Path (ETP)** when “it looks like a chain” and all *clocks are reset on the last transition*

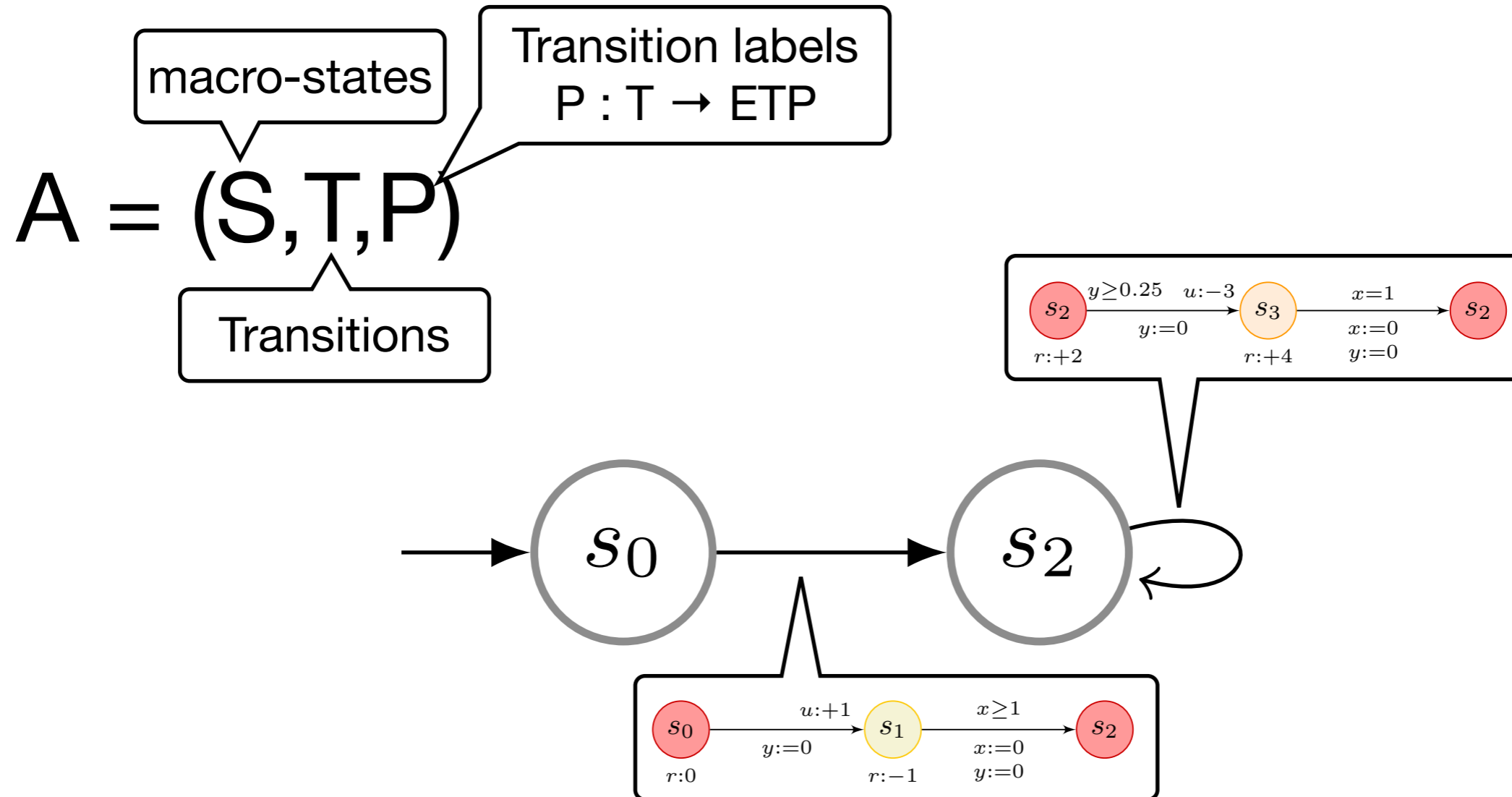
Energy Timed Automata



An ETA generates runs (i.e., sequences of configurations) describing how the clocks and the energy level evolves over time



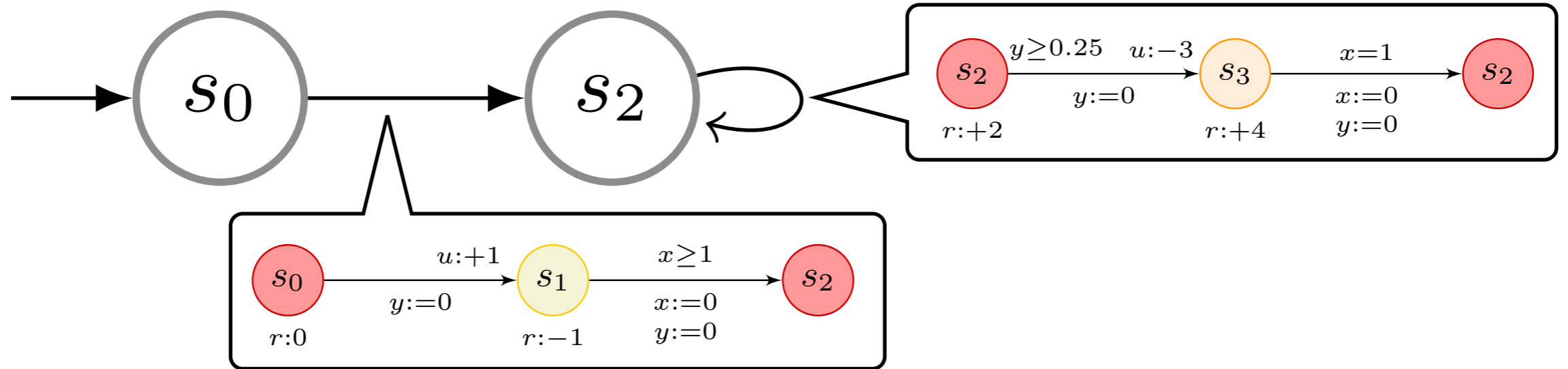
Segmented ETA



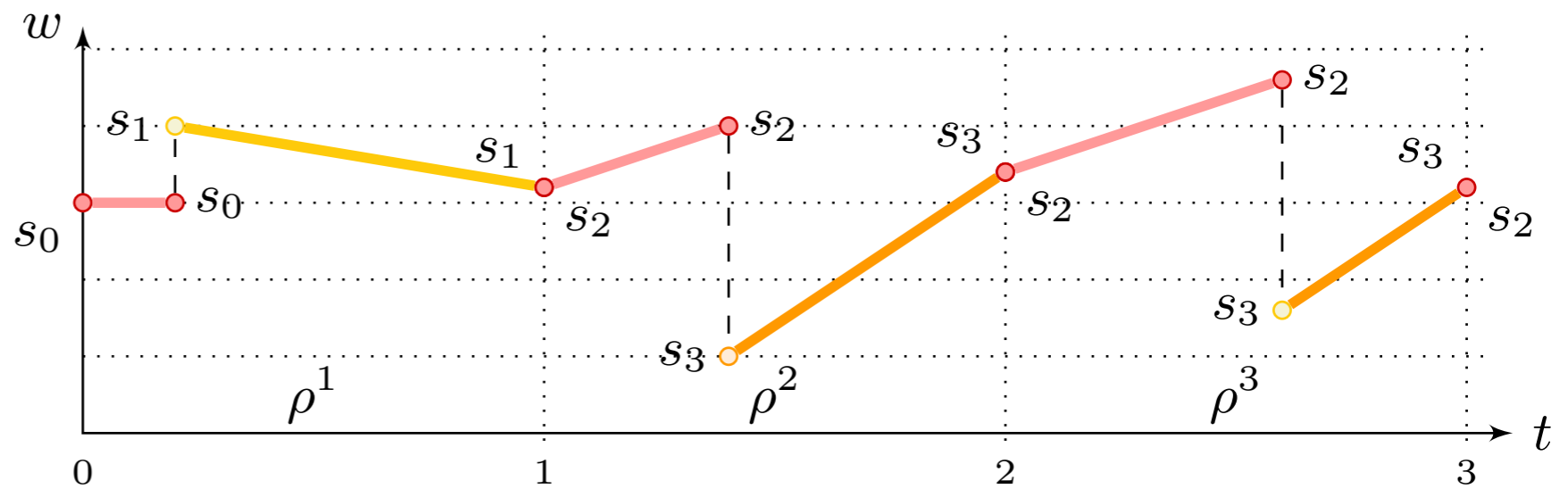
A SETA is called

- **flat** when for each $s \in S$ there is at most one path from s to itself.
- **depth-1** whenever the graph is tree-like with only loops at leaves

Segmented ETA



A finite (resp., infinite) execution of a SETA is a finite (resp., infinite) sequence of finite runs generated by its ETPs



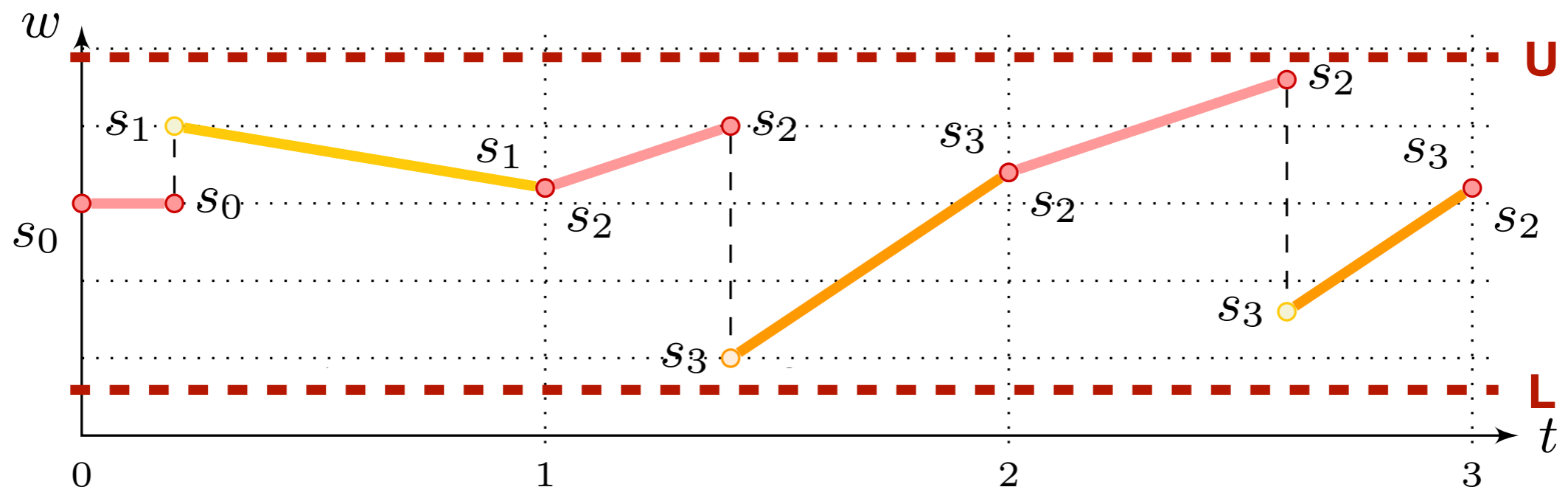
The energy-constrained infinite-run problem

INPUT

- An Energy timed automaton A
- Initial state s_0
- Initial energy level w_0
- Energy interval $E = [L, U]$

GOAL

Decide whether exists an **infinite execution** of A starting from $(s_0, 0, w_0)$ that **satisfies E**



The energy-constrained infinite-run problem

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GOAL

Decide whether exists an **infinite execution** of A starting from $(s_0, 0, w_0)$ **that satisfies E**

... what was known so far

Theorem [Markey'11]

The energy constrained infinite-run problem is **undecidable for ETAs with at least 2 clocks**

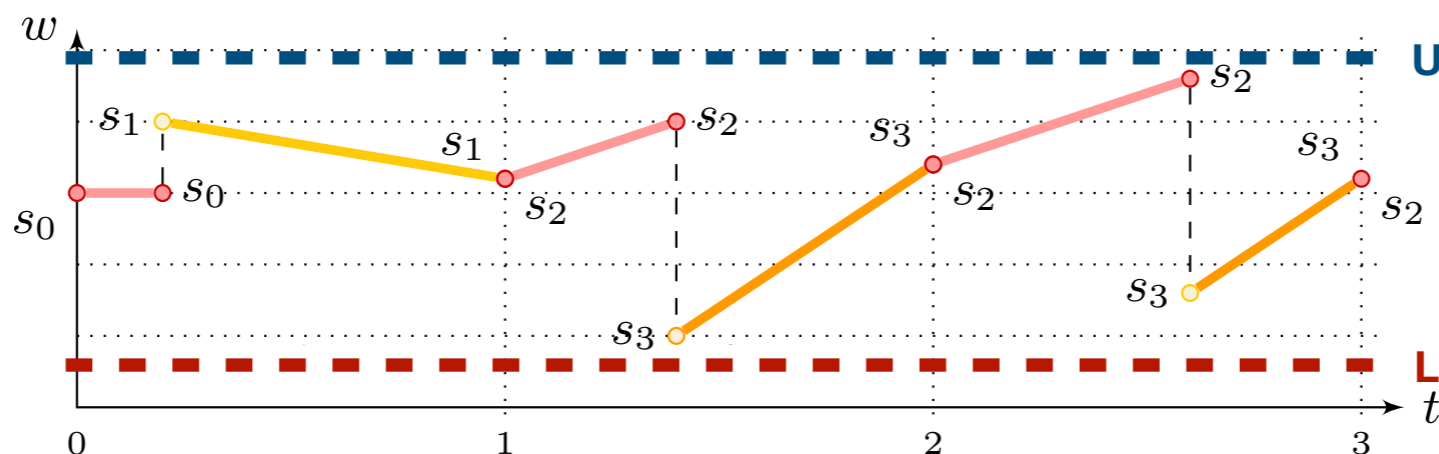
Our contribution to the problem

Theorem [Bacci et al. FM'18]

The energy-constrained infinite-run problem is **decidable for flat SETAs**

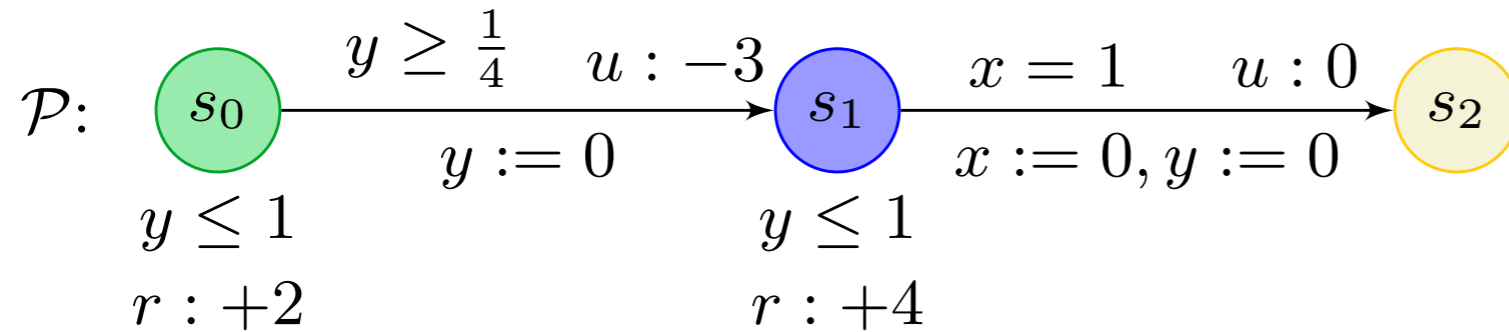
Theorem [Bacci et al. FM'18]

For a fixed **lower bound L** , **the existence of an energy upper bound U** that solves the energy-constrained infinite run problem is decidable for flat SETA.
For depth-1 flat SETA we can compute the least U .



The idea behind

Consider an Energy Timed Path



$$E = [0;5]$$

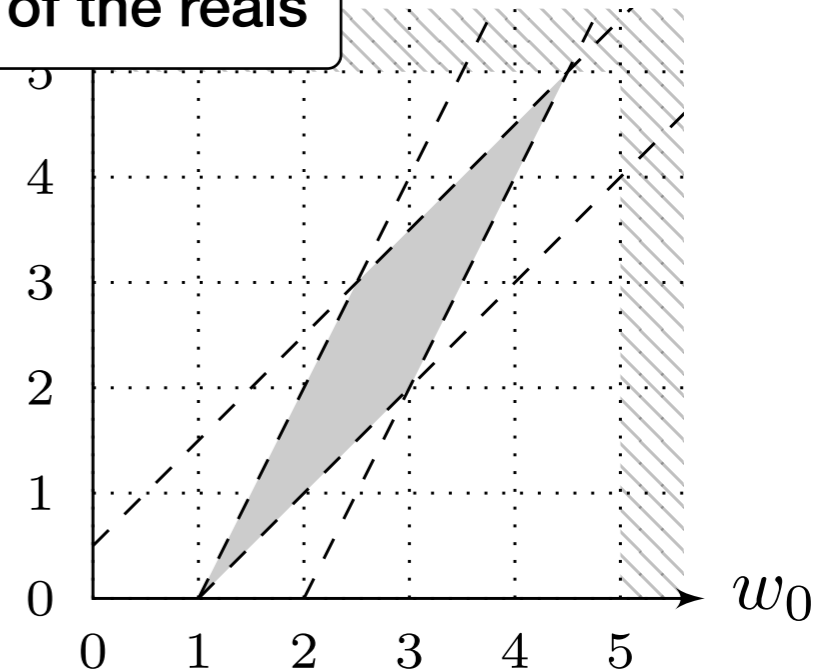
$$\mathcal{R}_{\mathcal{P}}^E(w_0, w_1)$$

Def.

$$\begin{aligned} \exists d_0, d_1. & d_0 \in [0.25; 1] \wedge d_1 \in [0; 1] \wedge d_0 + d_1 = 1 \wedge \\ & w_0 \in [0; 5] \wedge w_0 + 2d_0 \in [0; 5] \wedge w_0 + 2d_0 - 3 \in [0; 5] \wedge \\ & w_1 = w_0 + 2d_0 + 4d_1 - 3 \wedge w_1 \in [0; 5]. \end{aligned}$$

$$(w_1 + 2 \leq 2w_0 \leq w_1 + 4) \wedge (w_1 - 0.5 \leq w_0 \leq w_1 + 1)$$

Translation into a first-order formula in the linear theory of the reals



Quantifier elimination

The Energy Relation

Energy Relation

$$\mathcal{R}_{\mathcal{P}}^E(w_0, w_1) \iff \exists (d_i)_{0 \leq i < n} \cdot \Phi_{\text{timing}} \wedge \Phi_{\text{energy}} \wedge w_1 = w_0 + \sum_{k=0}^{n-1} (d_k \cdot r(s_k) + u_k)$$

Energy Functions

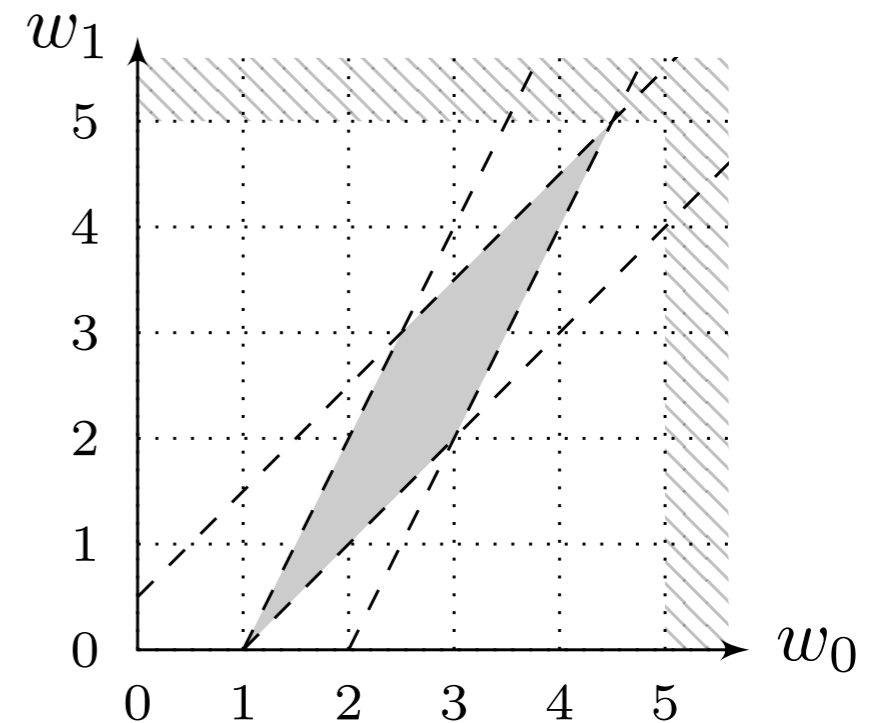
(*) Indices are removed to shorten notation

Forward propagation

$$\mathcal{R}(I) = \{w_1 \in E \mid \exists w_0 \in I. \mathcal{R}(w_0, w_1)\}$$

Backward propagation

$$\mathcal{R}^{-1}(I) = \{w_0 \in E \mid \exists w_1 \in I. \mathcal{R}(w_0, w_1)\}$$



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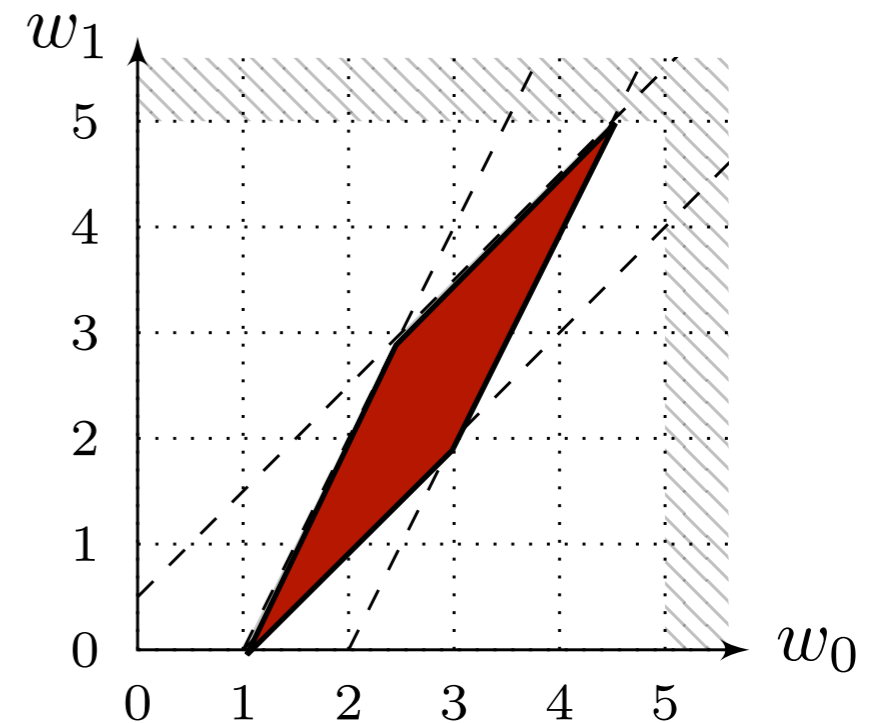
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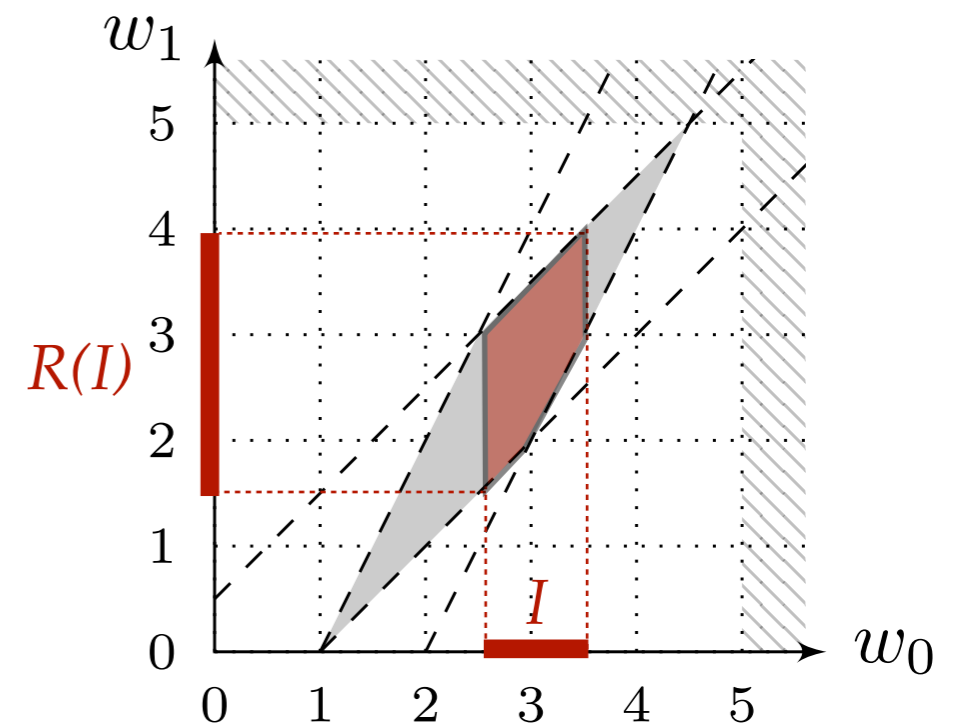
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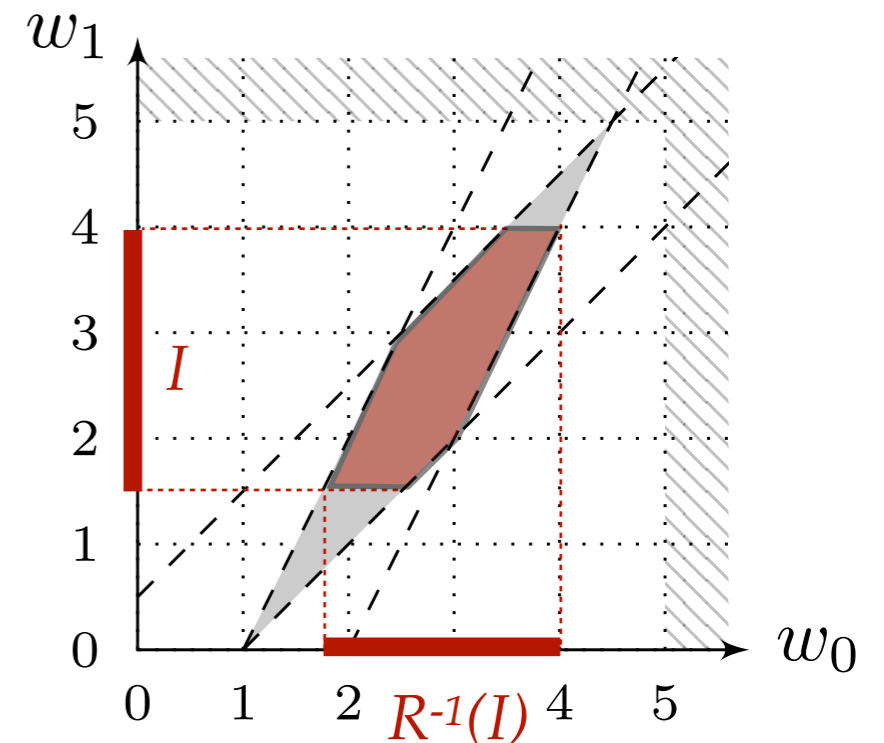
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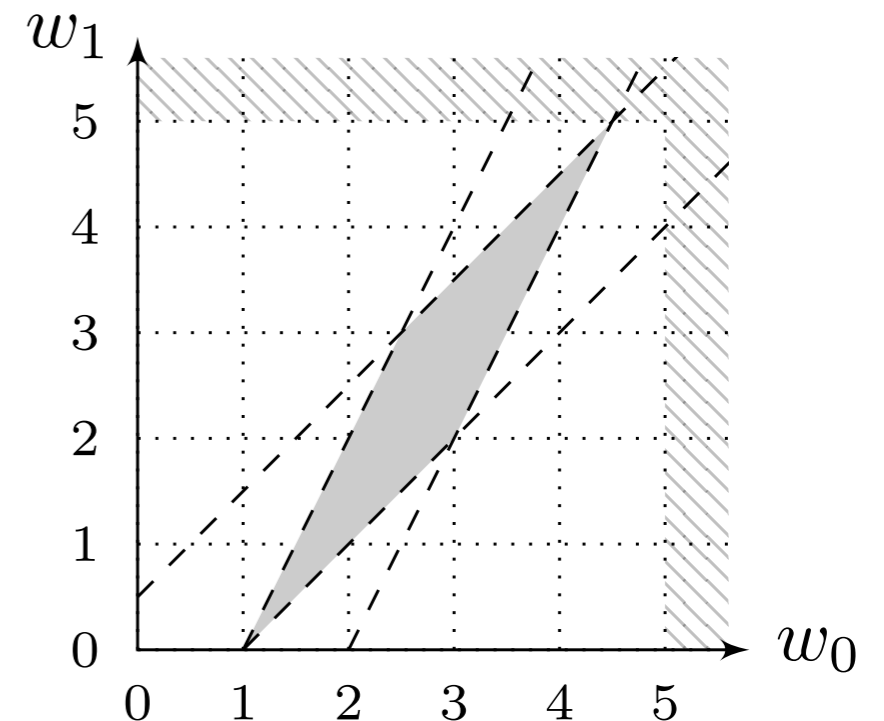
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Consider a finite sequence of ETAs $(\mathcal{P}_i)_{1 \leq i \leq k}$

$$\mathcal{R}_{\mathcal{P}}^E = \mathcal{R}_{\mathcal{P}_k}^E \circ \dots \circ \mathcal{R}_{\mathcal{P}_1}^E$$

Described as a
finite conjunction of
linear constraints over
 w_0 and w_1

From R to infinite runs

Consider a finite sequence of ETAs $(\mathcal{P}_i)_{1 \leq i \leq k}$ **forming a cycle**

$$\mathcal{R}_{\mathcal{P}}^E = \mathcal{R}_{\mathcal{P}_k}^E \circ \cdots \circ \mathcal{R}_{\mathcal{P}_1}^E$$

A post-fixed point for \mathcal{R}^{-1} is a set of initial energy values that can be forward propagated infinitely many times.

In particular, **the greatest fixed point contains all the initial energy values that admit an infinite run satisfying E**

$$\nu \mathcal{R}^{-1} = \bigcap_{i \in \mathbb{N}} (\mathcal{R}^{-1})^i (E)$$

Characterising $\nu\mathcal{R}^{-1}$

$$\nu\mathcal{R}^{-1} = \bigcap_{i \in \mathbb{N}} (\mathcal{R}^{-1})^i (E)$$

A generic post-fixed point $[a; b]$ is logically characterised as follows

$$\phi(a, b) := a \leq b \wedge a \in E \wedge b \in E \wedge$$

$$\forall w_0 \in [a; b]. \exists w_1 \in [a; b]. \mathcal{R}_P^E(w_0, w_1)$$

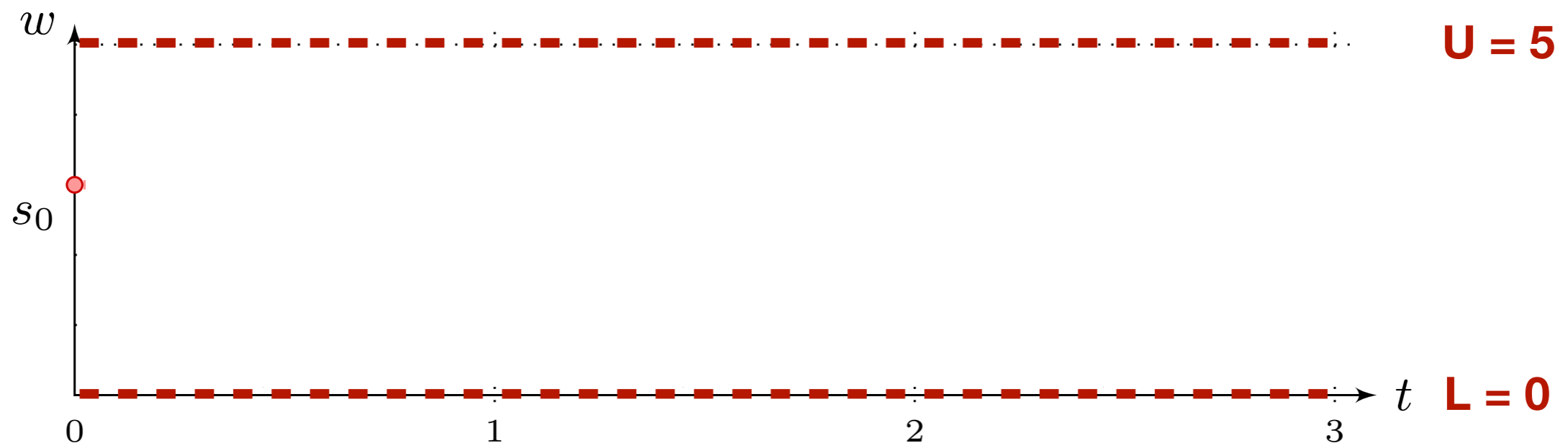
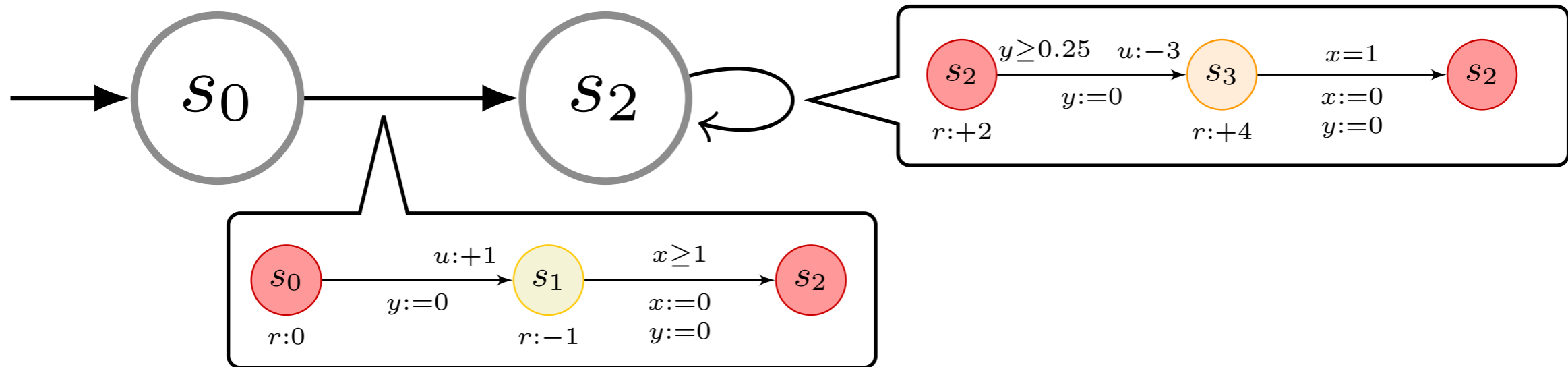
By applying **quantifier elimination** (to w_0 and w_1) the above formula may be transformed in a finite disjunction of linear constraints, thus

$$\max_{a, b} \{b - a \mid \phi(a, b) \text{ holds}\}$$

This gives a method for computing $\nu\mathcal{R}^{-1}$

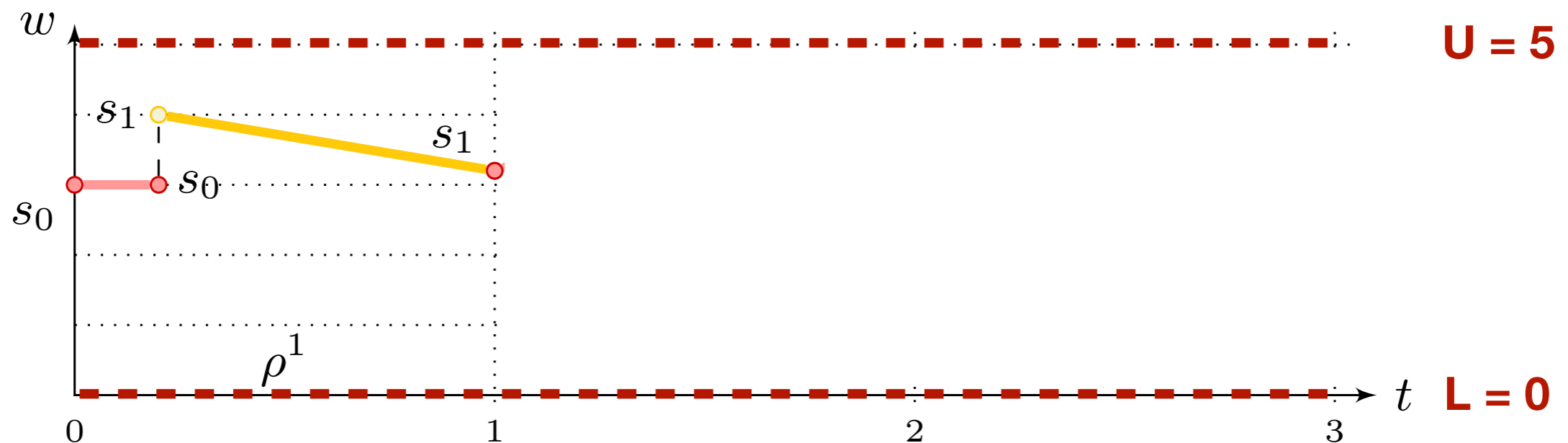
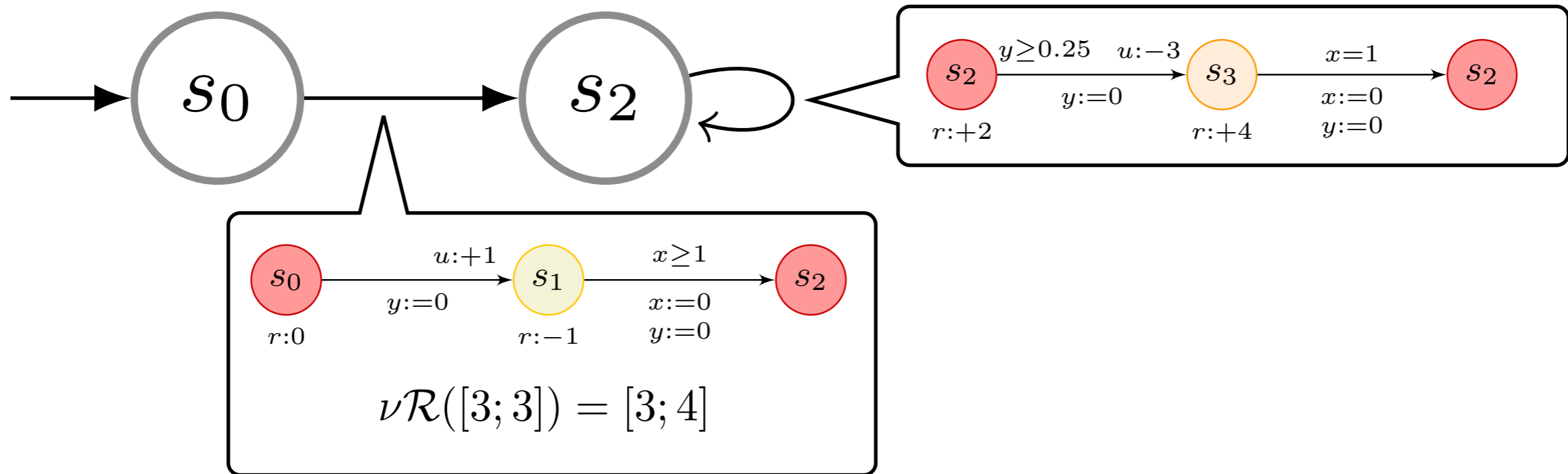
Finding an infinite-run in a SETA

Consider the initial energy $w_0 = 3$ and the energy interval $E = [0; 5]$



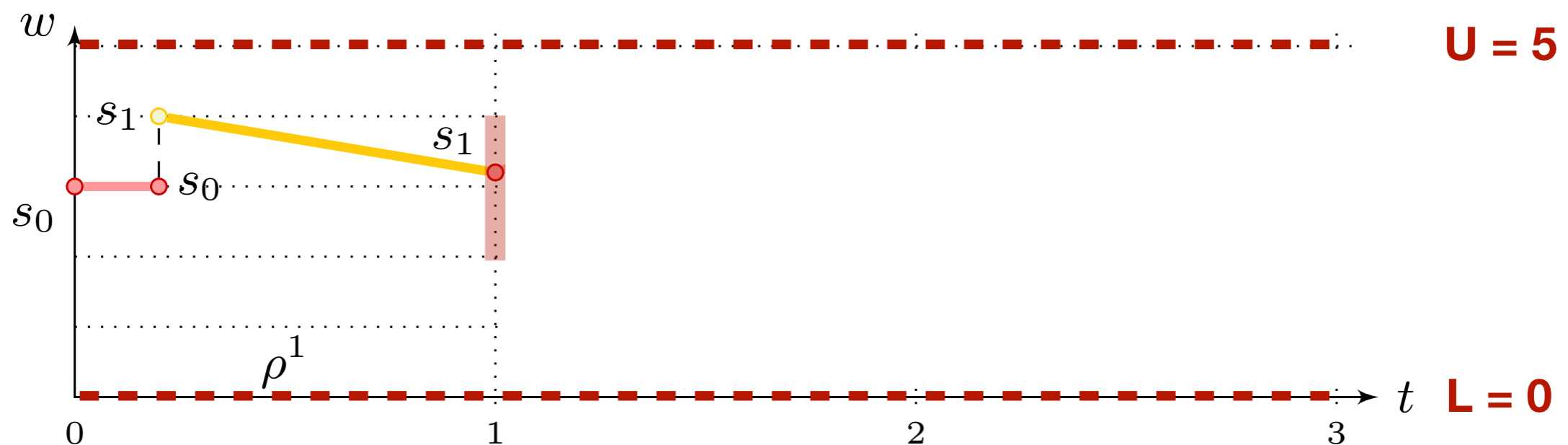
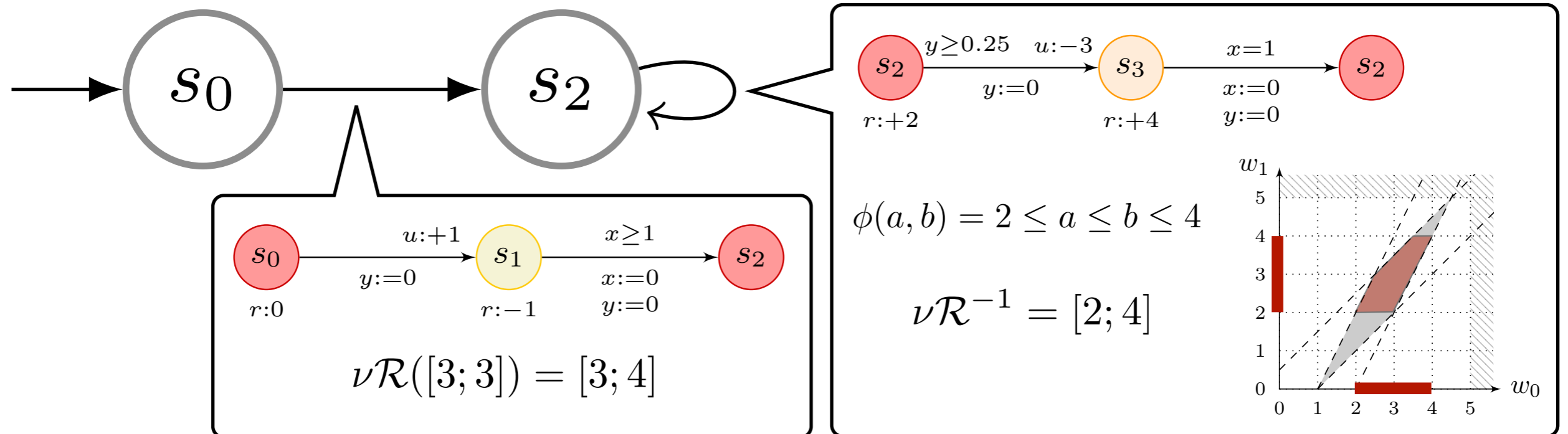
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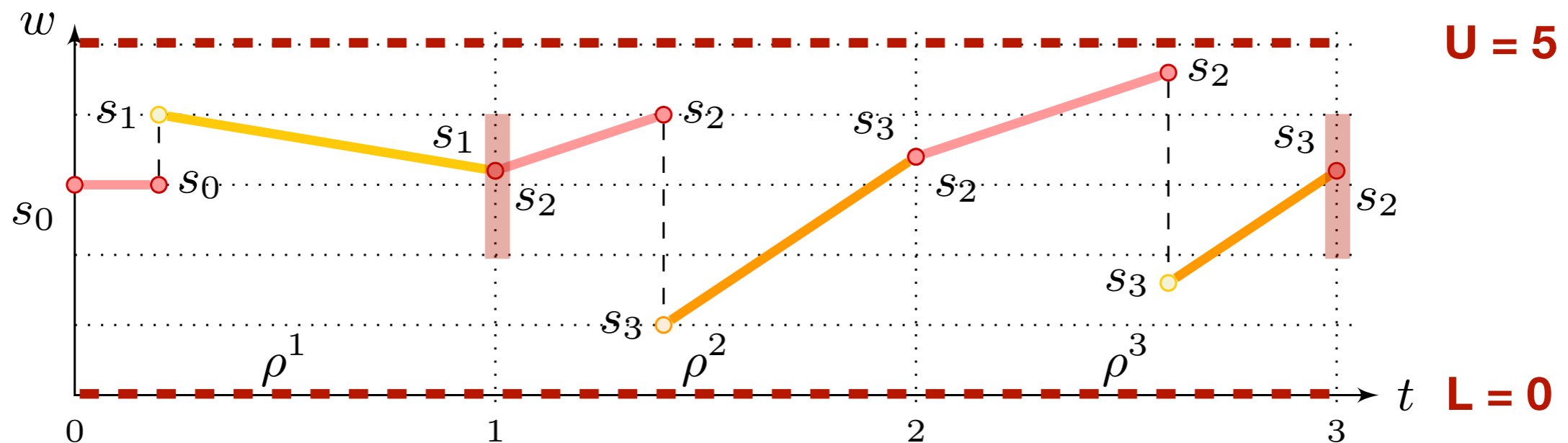
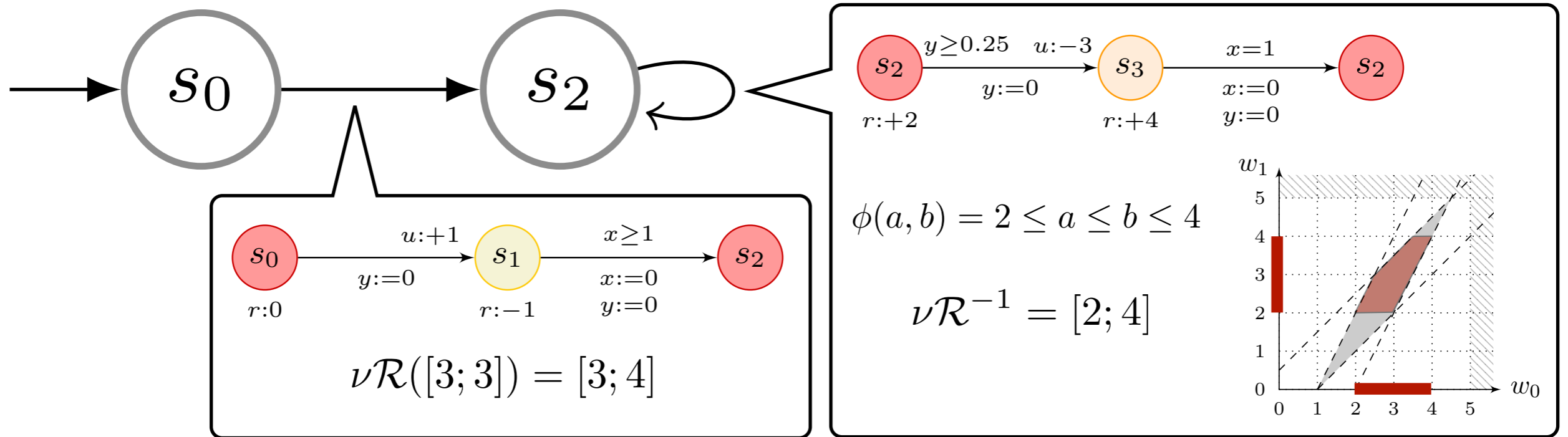
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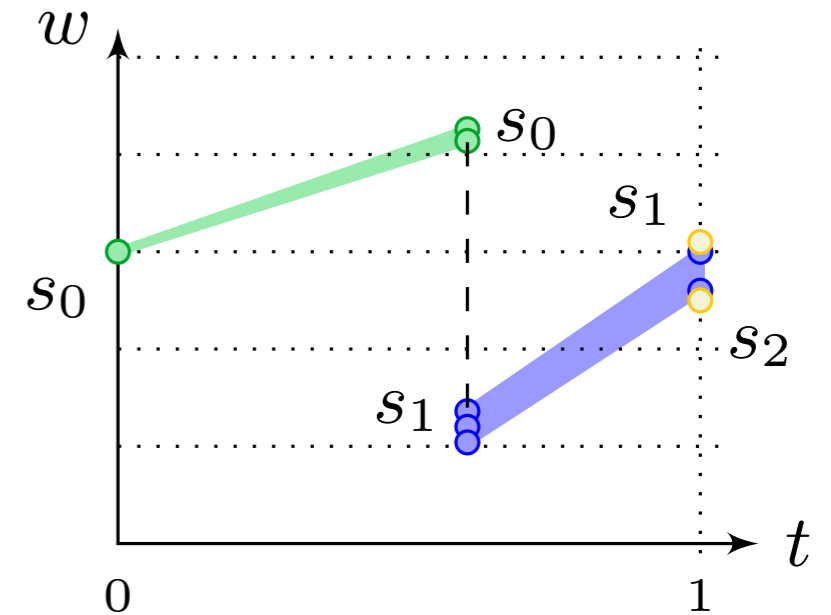
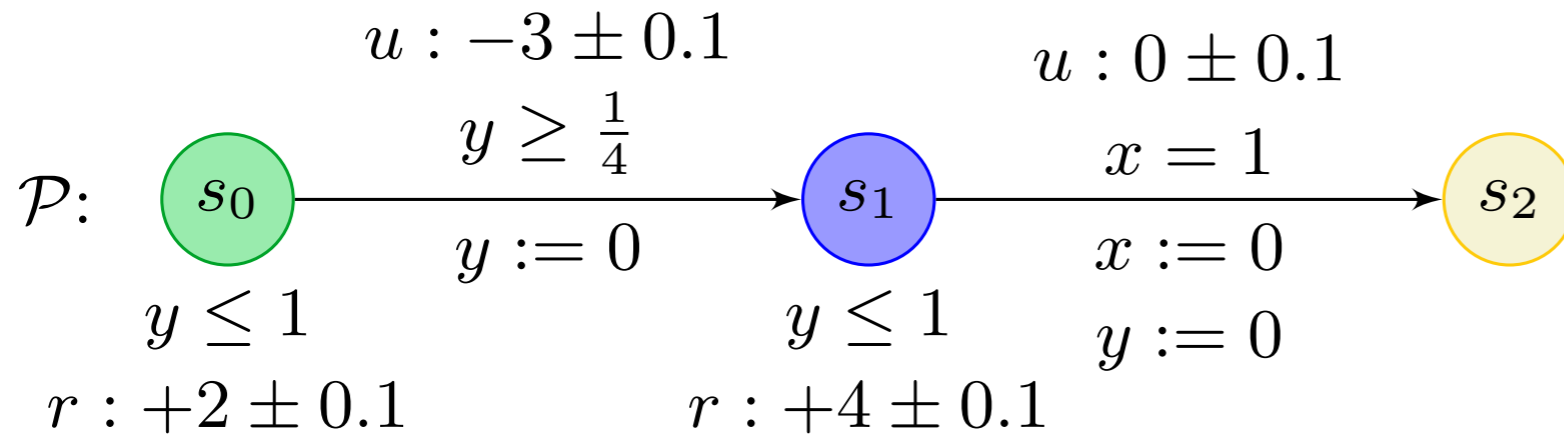


Finding an infinite-run in a SETA

Consider the initial energy $w_0 = 3$ and the energy interval $E = [0; 5]$



Adding uncertainty to ETA



$$\begin{aligned}
 \mathcal{U}_{\mathcal{P}}^E(w_0, a, b) &\iff \exists d_0, d_1. d_0 \in [0.25; 1] \wedge d_1 \in [0; 1] \wedge d_0 + d_1 = 1 \wedge w_0 \in [0; 5] \wedge \\
 &w_0 + [1.9; 2.1] \cdot d_0 \subseteq [0; 5] \wedge \\
 &w_0 + [1.9; 2.1] \cdot d_0 + [-3.1; -2.9] \subseteq [0; 5] \wedge \\
 &w_0 + [1.9; 2.1] \cdot d_0 + [-3.1; -2.9] + [3.9; 4.1] \cdot d_1 \subseteq [0; 5] \wedge \\
 &w_0 + [1.9; 2.1] \cdot d_0 + [-3.1; -2.9] + [3.9; 4.1] \cdot d_1 + [-0.1; 0.1] \subseteq [a; b] \subseteq [0; 5]
 \end{aligned}$$

\updownarrow
 QE

$$\begin{aligned}
 0 \leq a \leq b \leq 5 \wedge b \geq a + 0.6 \wedge a - 0.2 \leq w_0 \leq b + 0.7 \wedge \\
 (4.87 + 1.9 \cdot a)/3.9 \leq w_0 \leq (7.27 + 2.1 \cdot b)/4.1
 \end{aligned}$$

The (ternary) energy relation takes into account all possible energy outcomes

Our contribution to the problem

Theorem [Bacci et al. FM'18]

The energy-constrained infinite-run problem is **decidable for SETAu satisfying (R)**

We do not require flatness!

(R) in any ETPu of the SETAu some clock is compared with a positive lower bound. Thus, there is an (overall minimal) positive time-duration D to complete any ETAu.

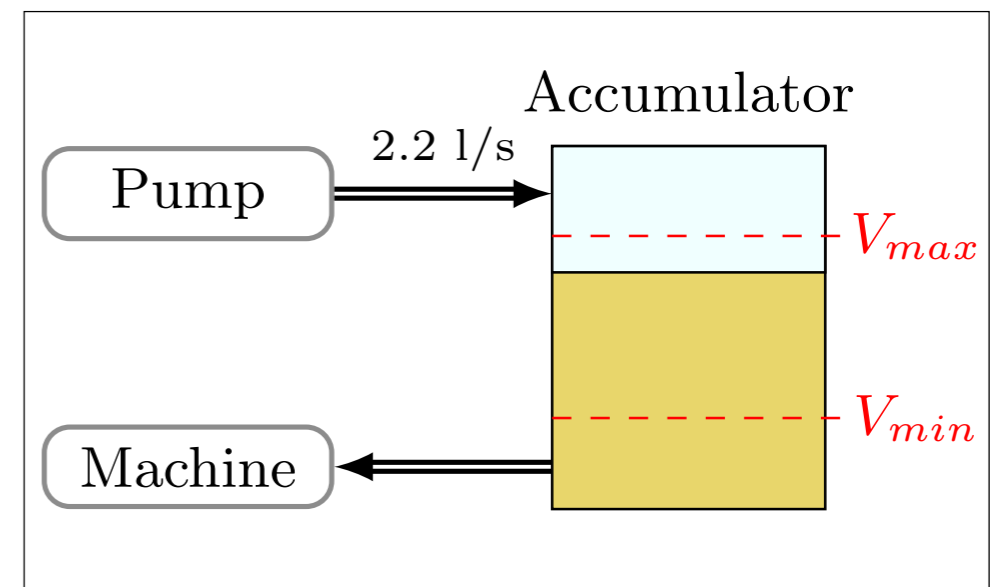
Theorem [Bacci et al. FM'18]

For a fixed **lower bound L** , **the existence of an energy upper bound U** that solves the energy-constrained infinite run problem is decidable for **depth-1 flat SETAu**.
Furthermore, **we can compute the least U** .

Back to the Case Study: the HYDAC system

System components

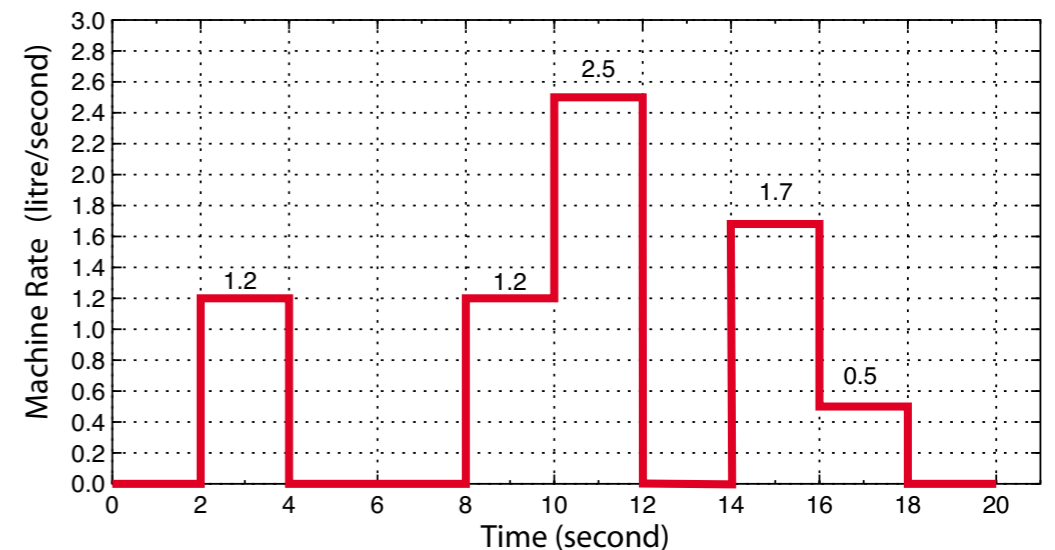
- A **machine** that consumes oil according to a **fixed cyclic pattern of 20s**
- Hydraulic **accumulator** containing oil and a fixed amount of gas that puts the oil under pressure
- **Controllable pump (on/off)** which **pumps oil** into the accumulator **with rate 2.2 l/s**



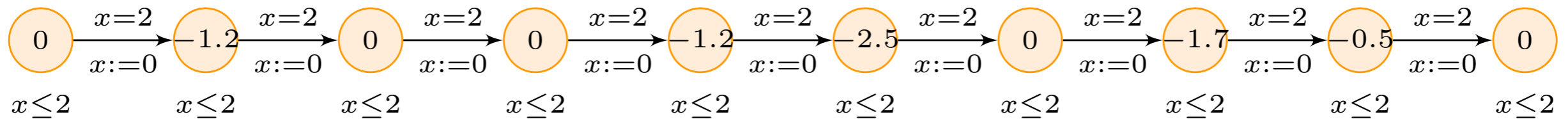
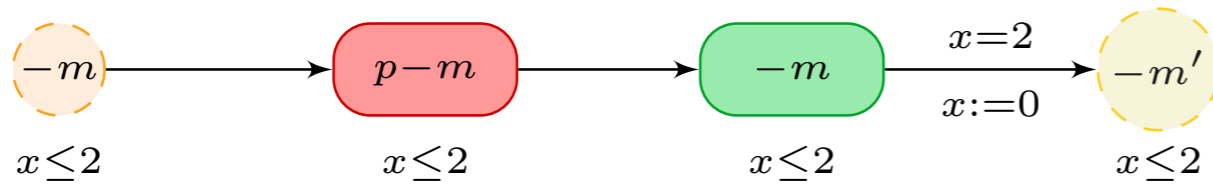
The control objective

- The level of oil shall be maintained within a **safe interval $[V_{max}; V_{min}] = [4.9; 25.1]$ l**
- The **system shall never stop**
- **Minimise the average level of oil**

$$\int_{t=0}^{t=T} \frac{v(t)}{T} dt$$



Modelling the HYDAC system

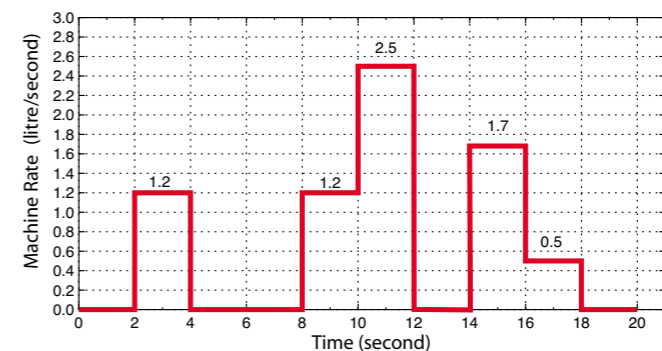


The parallel composition of the two ETPs
Models the system precisely, however it is not a flat-SETA

We propose two variants of the system:

- **H_1 allows the pump to switch once every 2-sec slot**
- **H_2 allows the pump to switch once every second 2-sec slot**

ETP modelling a machine cycle



We consider also extensions $H_1(\epsilon)$ and $H_2(\epsilon)$ with uncertainty $\epsilon = 0.1$ l/s

Machine consumption rate $[-m - \epsilon, -m + \epsilon]$

Synthesising Controllers

- **Synthesis of optimal energy bounds**

- A. synthesise the **minimal upper bound U** admitting an infinite run satisfying the energy interval $[V_{\min}, U]$
- B. Determine the **greatest safe energy interval** $[a,b] \subseteq [V_{\min}, U]$

- **Synthesis of optimal safe strategies**

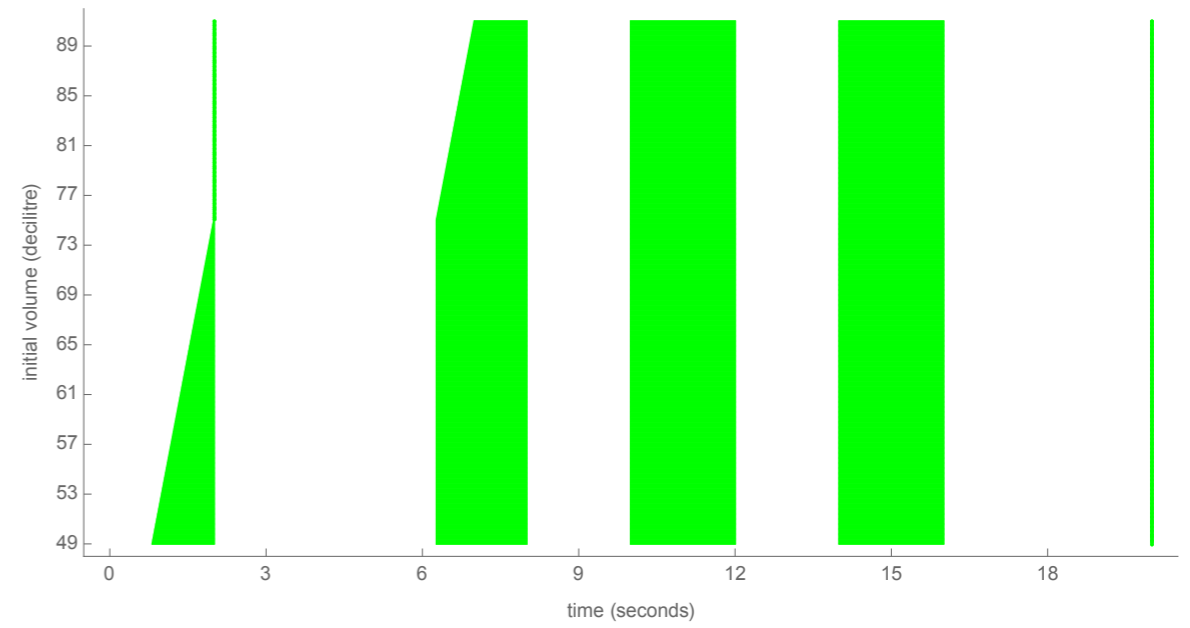
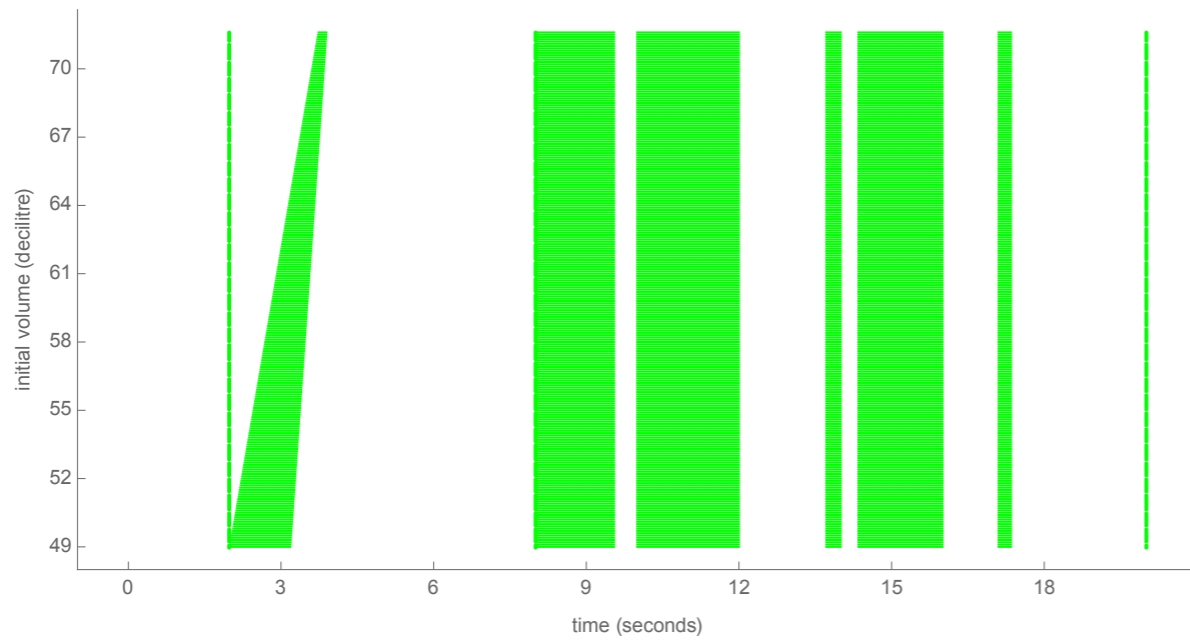
1. The set of **permissive strategies** is modelled as a quantifier-free first-order formula
2. Minimise the (non-linear) cost function $\int_{t=0}^{t=T} \frac{v(t)}{T} dt$ expressing the average oil volume

Synthesised Controllers

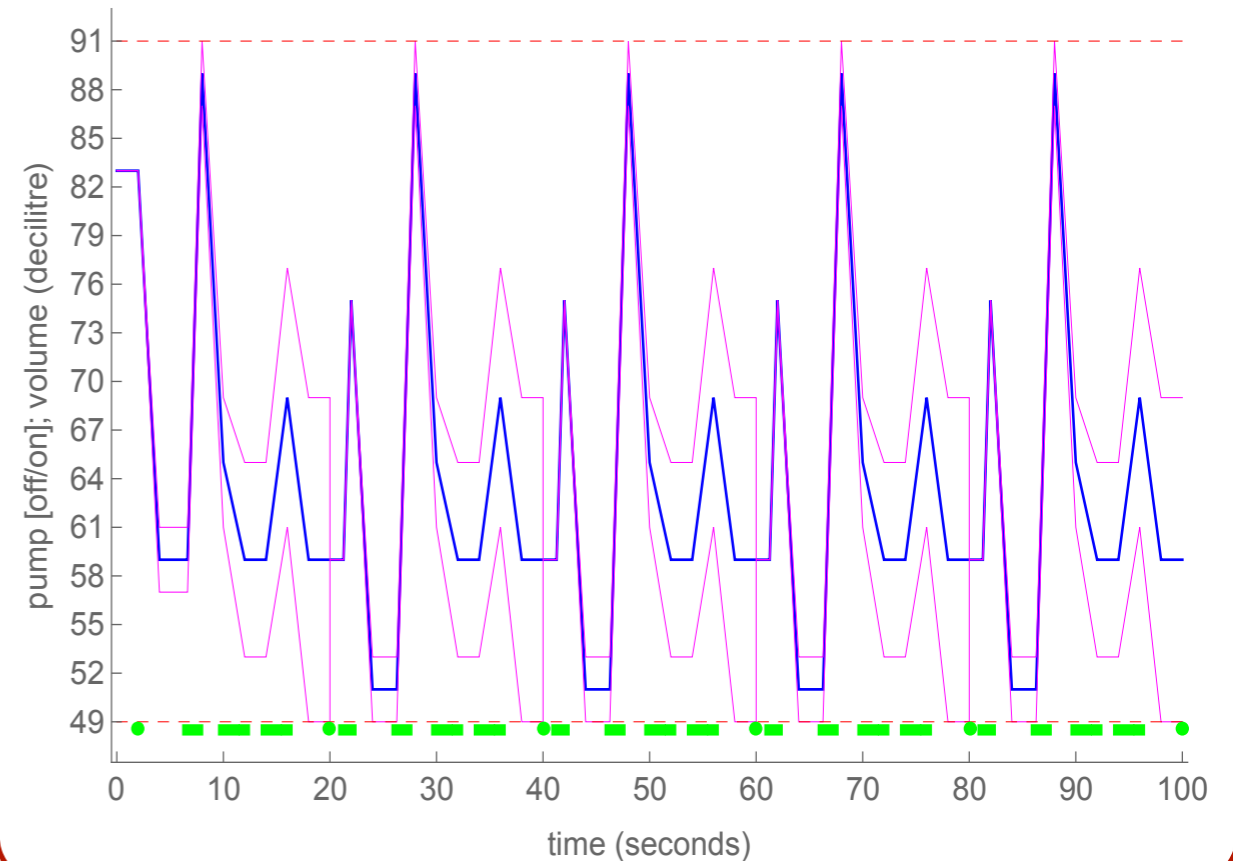
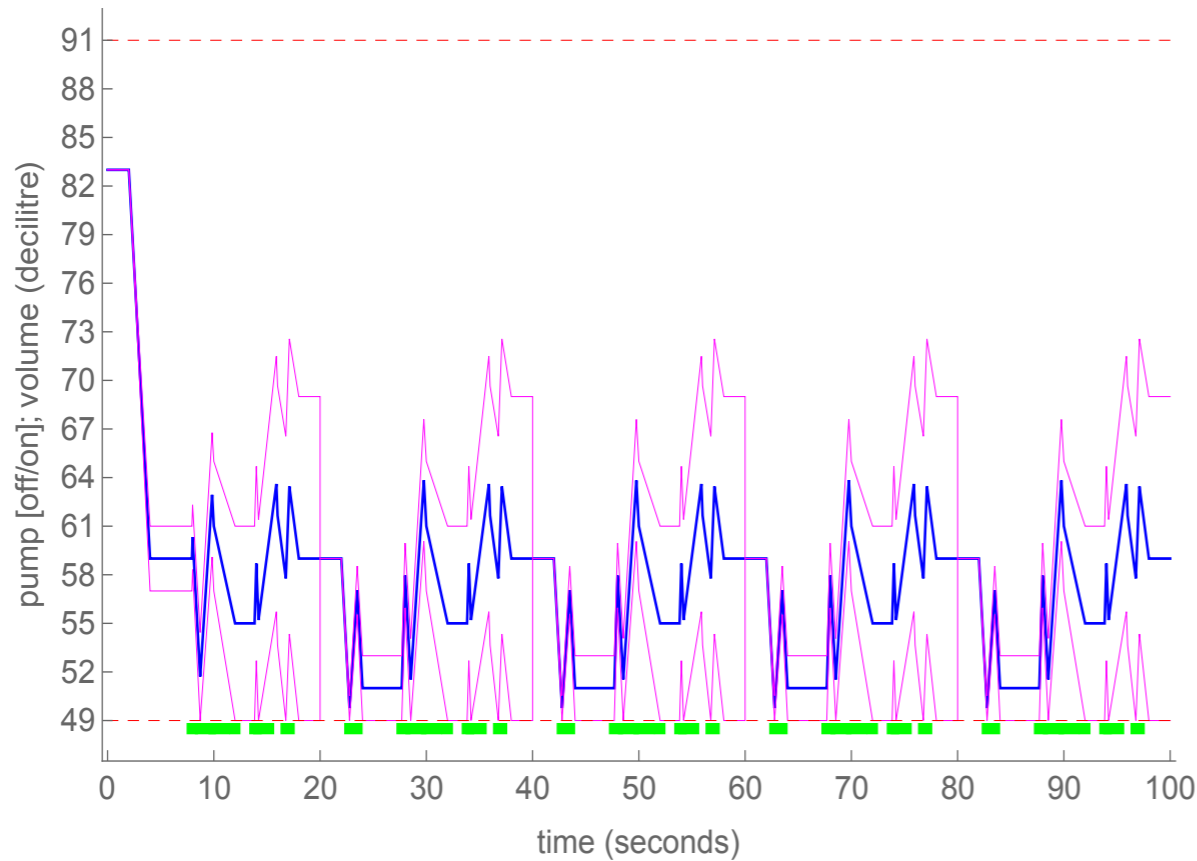
$H_1(\epsilon)$

$H_2(\epsilon)$

Local controller



Simulation (10 cycles)



Performance

Controller	$[L; U]$	$[a; b]$	Mean vol. (l)
\mathcal{H}_1	[4.9; 5.84]	[4.9; 5.84]	5.43
$\mathcal{H}_1(\epsilon)$	[4.9; 7.16]	[5.1; 7.16]	6.15
\mathcal{H}_2	[4.9; 7.9]	[4.9; 7.9]	6.12
$\mathcal{H}_2(\epsilon)$	[4.9; 9.1]	[5.1; 9.1]	7.24
G1M1 [16]	[4.9; 25.1] ^(*)	[5.1; 9.4]	8.2
G2M1 [16]	[4.9; 25.1] ^(*)	[5.1; 8.3]	7.95
[29]	[4.9; 25.1] ^(*)	[5.2; 8.1]	7.35

Tool Chain:

- *Mathematica* (constr & simpl)
- *Mjollnir* (QE)

Compositional Methods:

20 min → 20 ms

^(*) Safety interval given by the HYDAC company.

Controller	Acc. vol. (l)	Mean vol. (l)	Controller	Acc. vol. (l)	Mean vol. (l)
\mathcal{H}_1	1081.77	5.41	Bang-Bang	2689	13.45
\mathcal{H}_2	1158.90	5.79	HYDAC	2232	11.60
$\mathcal{H}_1(\epsilon)$	1200.21	6.00	G1M1	1518	7.59
$\mathcal{H}_2(\epsilon)$	1323.42	6.62	G2M1	1489	7.44

[16] Cassez, Jensen, Larsen, Raskin, Reyner - Automatic Synthesis of Robust and Optimal Controllers (HSCC'09)

[29] Zhao, Zhan, Kapur, Larsen - A "hybrid" approach for synthesising optimal controllers of hybrid systems: A case study of the oil pump industrial example (FM'12)

Conclusion

- Novel framework for synthesis of safe and optimal controllers, based on energy timed automata.
- Approach based on
 1. translation into first-order formulas in the linear theory of the reals
 2. quantifier elimination
 3. Numerical optimisation
- Applicable on real industrial applications
- Prototype tool using Mathematica & Mjollnir (available at <http://people.cs.aau.dk/~giovbacci/tools.html>)

Future Work

- Extend the result to (non-flat) and non-segmented ETAs
- Add UPPAAL STRATEGO to our tool chain

Thank you

Synthesising Controllers

Synthesis of optimal energy bounds

We **synthesise a minimal upper bound U^*** (within the interval $E = [V_{min}, V_{max}]$) admitting an infinite run satisfying the energy interval $E' = [V_{min}, U^*]$

$$\min \left\{ U \mid V_{min} \leq a \leq b \leq U \leq V_{max} \wedge \forall w_0 \in [a, b]. \exists w_1 \in [a, b]. \mathcal{R}_{\mathcal{P}}^{[V_{min}, U]}(w_0, w_1) \right\}$$

We compute the **greatest energy-safe interval $[a, b] \subseteq E'$**

$$\max \left\{ b - a \mid V_{min} \leq a \leq b \leq U^* \wedge \forall w_0 \in [a, b]. \exists w_1 \in [a, b]. \mathcal{R}_{\mathcal{P}}^{E'}(w_0, w_1) \right\}$$

Synthesis of optimal safe strategy

The set of **permissive strategies** is described as a quantifier-free first-order formula

$$\Phi_{on} \wedge \Phi_{off} \wedge \Phi_{timing} \wedge \Phi_{energy} \wedge w_1 = w_0 + \sum_{k=0}^{n-1} (d_k \cdot r(s_k) + u_k)$$

An optimal strategy is a permissive strategy that **minimise the non-linear cost function expressing the average oil volume**